

Average values of  $h_1 - h_2 = 2.53$  mm and  $h_2 - h_5 = 0.47$  mm were found for a 190-kbar shock in 12-mm-thick samples of iron.<sup>25</sup> If  $U_2' = 3.578$  mm/ $\mu$ sec,  $R_2' = 5.69$  mm/ $\mu$ sec, and  $R_1' = 6.58$  mm/ $\mu$ sec, then  $h_2 - h_3 = .98$  mm which is equivalent to a rise time of 0.27  $\mu$ sec for the plastic II wave front. This value is within the range of observed values of rise time described in the preceding section, but near the high side.

### 6.2. Slow Decay of the Stress Behind the Plastic I Shock

It was noted in Chapter 4 that  $P^{TL}$  diminishes slowly with propagation distance; but that if stress jump across the plastic I front is considered, this slow decay disappears. Therefore, one can reasonably infer that the slow decay of  $P^{TL}$  is due to precursor decay. The situation can be complicated by wave interactions so the inference is not conclusive.

The situation can be clarified by describing possible bounds of stress-particle velocity states at the impact boundary when an iron sample is impacted by an aluminum projectile. Figure 6.4 illustrates the pressure-particle velocity plane; dashed lines represent metastable extensions of lower pressure states and the solid lines represent equilibrium Hugoniot. The aluminum cross curve represents possible states at the impact boundary. Point A represents the maximum attainable stress at the instant of impact, and C represents the equilibrium stress obtained when all time effects have disappeared. The problem of kinetics at the impact surface is to describe how fast the stress gets from A to C. The time required for stress to decay from

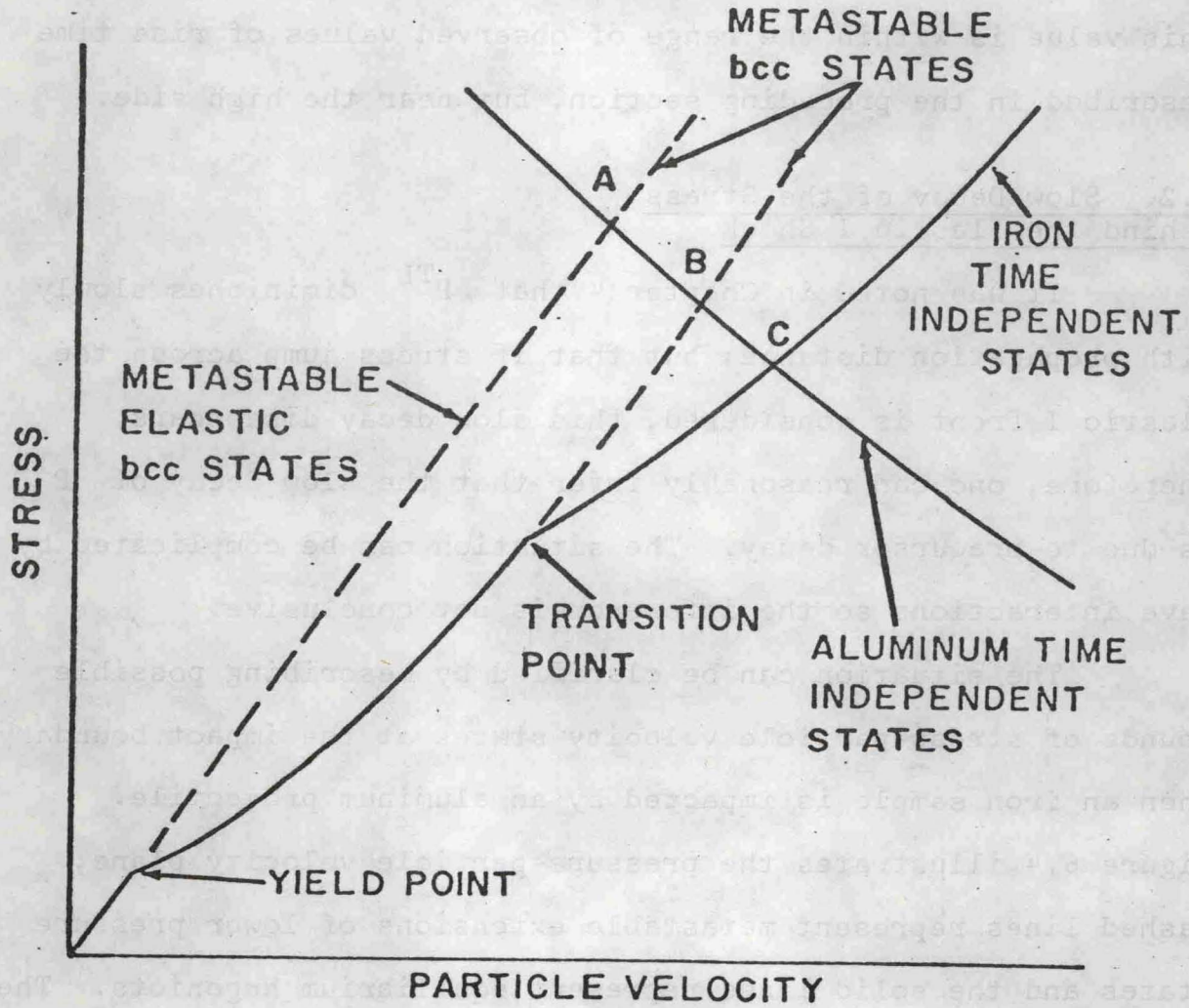


Fig. 6.4.--Stress-particle velocity states at the impact boundary when an iron sample is impacted by an aluminum plate.